

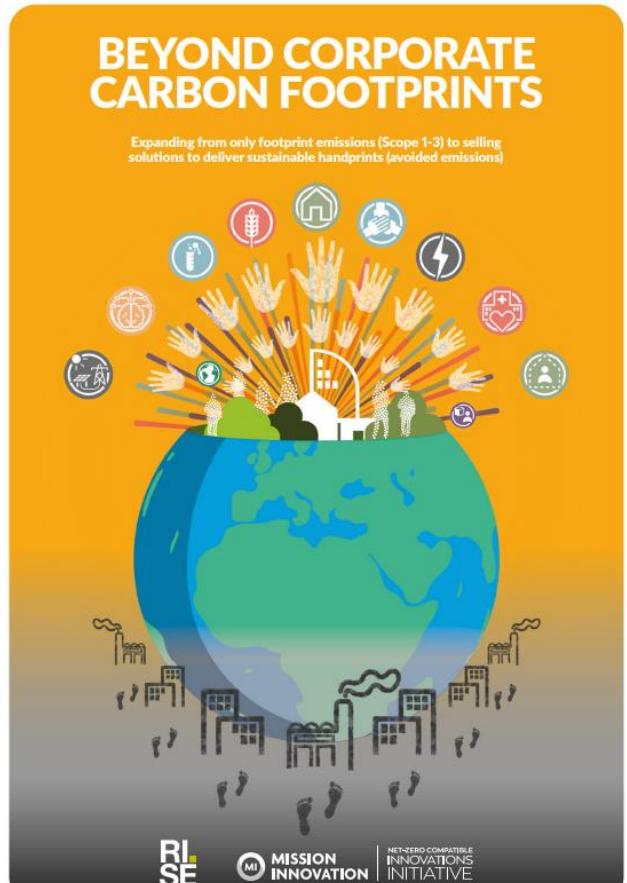
Sustainable PUR material and products

Nazdaneh Yarahmadi,
nazdaneh.yarahmadi@ri.se

Tel: 0705495921
0105165921

RISE Research Institutes of Sweden

Sustainable PUR material and products



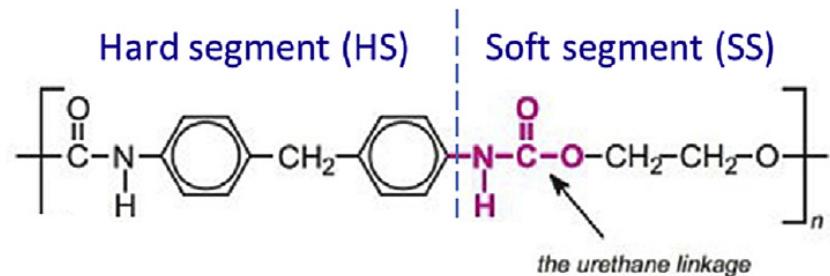
Focus has been on reduction of emissions from companies and their value chains. Most tools and initiatives have therefore focused on measuring and reporting emissions from value chain emissions.

Incentive structures have been developed based on the assumption that the best a company can do is reduce emissions and reach "Net-Zero".

The common denominator is that all of the above is based on a "**static reduction approach**", an approach where the large companies, the infrastructure and consumption patterns, are assumed as static and where improvements in existing systems is the focus.

Instead of the reduction of emissions from existing companies and structures that are inherently unsustainable, the main challenge from a long-term perspective is to avoid emissions and deliver on human needs with the help of innovative companies that can deliver what is needed in a sustainable way.

Sustainable PUR



Material: Biobased

Service life: Durable

End of life or circularity:
Recycling by
mechanical, chemical
and biological recycling
or reuse (such as
adsorbent)

“Starting materials, processes and characteristics of bio-based foams: A review”- Journal of Bioresources and bioproducts- Volume 9, Issue 2, may 2024

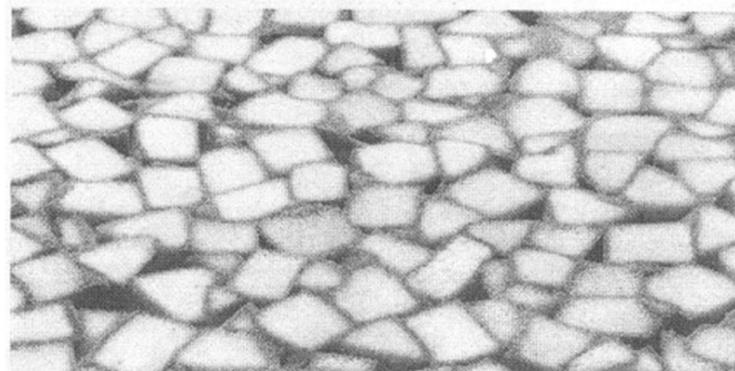
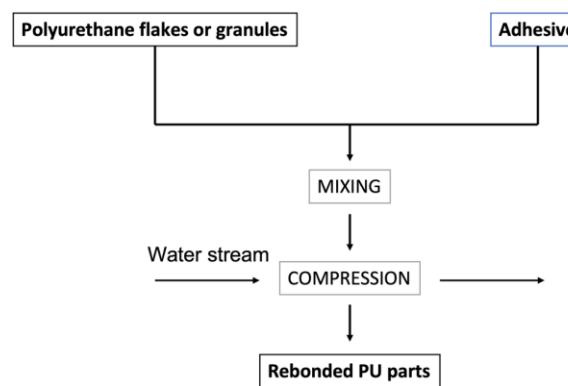
- Bio Polyol (vegetable oil, palm oil, soyabean oil, casteroil, etc. or waste from lignin from paper industry), lower reactivity compared with petroleum-based phenols.
- Bio Isocyanate (synthesize linear saturated terminal diisocyanate from oleic acid or vanilic acid derivate hydroxymethylfural (HMF) for reactive isocyanate monomer)

End of life or circularity:

Recycling by mechanical, chemical and biological recycling or reuse (such as adsorbent)

“Recycling of polyurethanes: where we are and where we are going”-Royal Society of Chemistry- Green Chem. 2024, v. 26 p.1132

- PU recycling *via* Mechanical recycling- represents the easiest and most basic strategy for thermoplastic PUR men problem of mechanical recycling is related to the degradation of the polymer properties after each recycling cycle, because of the degradation caused by reprocessing (thermo-mechanical degradation) that sums to the degradation during lifetime (thermo-oxidative one).

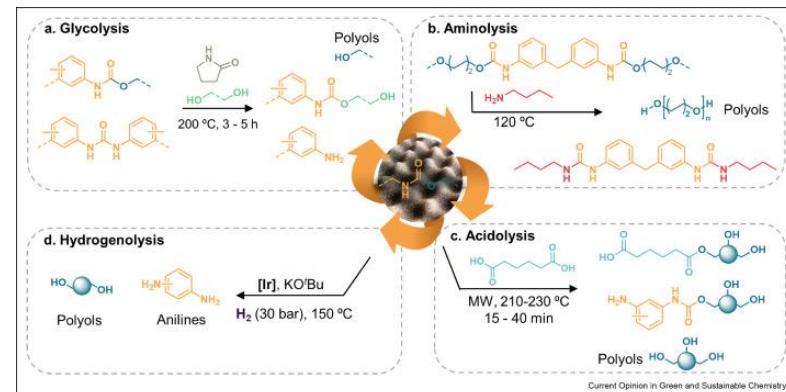


Rebonded foam: homogeneous distribution of the flake-binder mixture

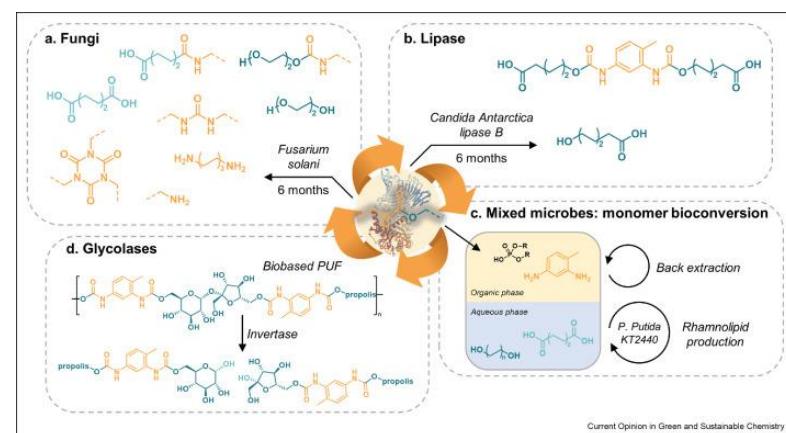
Sustainable PUs and reducing our reliance on fossil resources

“Reducing the carbon footprint of polyurethanes by chemical and biological depolymerization: Fact or fiction?” [Current Opinion in Green and Sustainable Chemistry, Volume 41, June 2023, 100802](#)

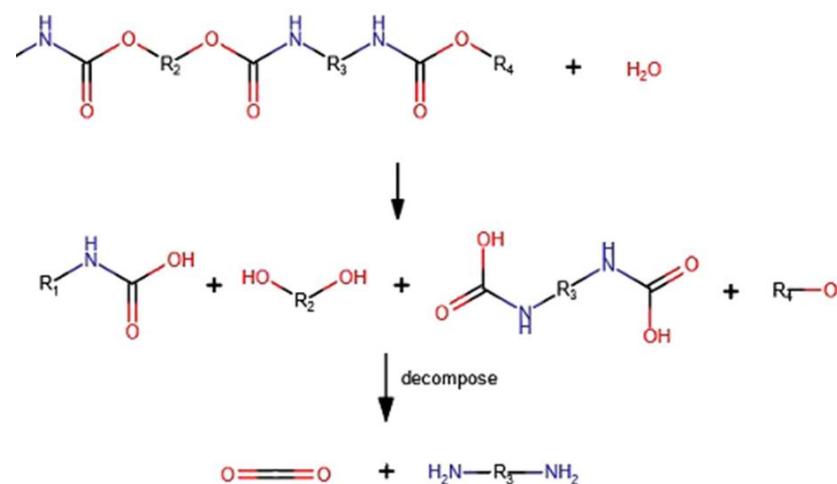
■ PU depolymerization via chemical catalysis



■ Depolymerization of PUs via biological catalysis



- Depolymerisation via biological catalysis or enzymatic degradation of PUs remains mainly limited to polyester-PUs.
- Chemical depolymerization:
 - the recovery of polyols (reused in a closed-loop recycling approach), low molar mass diols [e.g., ethylene glycol (EG), 1,4-butanediol (BDO)], diacids [e.g., succinic acid, adipic acid (AA)] or ω -hydroxy acids [e.g., 6-hydroxycaproic acid (6-HCA)], depending on the nature of the polyester polyol used.



Conclusion for recycling

Green Chem., 2024, 26, 1132,

the recycling strategies that have been designed and exploited so far, or are being developed for polyurethane waste streams,

- it is not possible to identify an ideal, unique, feasible, reliable, and even scalable recycling technology that should be suitable for all polyurethanes, but it is necessary to develop specific recycling approaches that maximize the yields, purity, and exploitability of the resulting recycled products, trying, at the same time, to minimize the environmental impact and the overall energy consumption

Reuse (such as adsorbent)

RISE earlier project- Development of Cost-Efficient CO₂ Adsorbents from Low-value Polymers

1. Background

2. Step 1 project—Proof of concept

3. Step 2 project (application)—Design and optimization



- Reach zero-net emission of greenhouse gases by 2045, and thereafter achieve net negative emissions.
- CO₂ emissions should reduce by 85 % compared to the level in 1991 (71 Mt CO₂eqv)
- CDR* measures should be applied to achieve negative emissions amounting to at least 10.7 Mt CO₂ per year by 2045.



*Carbon dioxide removal (CDR), also known as negative CO₂ emissions, is a process in which carbon dioxide gas (CO₂) is removed from the atmosphere and sequestered for long periods of time

Sweden's climate goals

100 kt/år < CO₂ utsläpp < 500 kt/år

Totala utsläpp (kton)

Cement Kraft/Värme

- 100-200
- ≤300
- ≤400
- ≤500
- 100-200
- ≤300
- ≤400
- ≤500

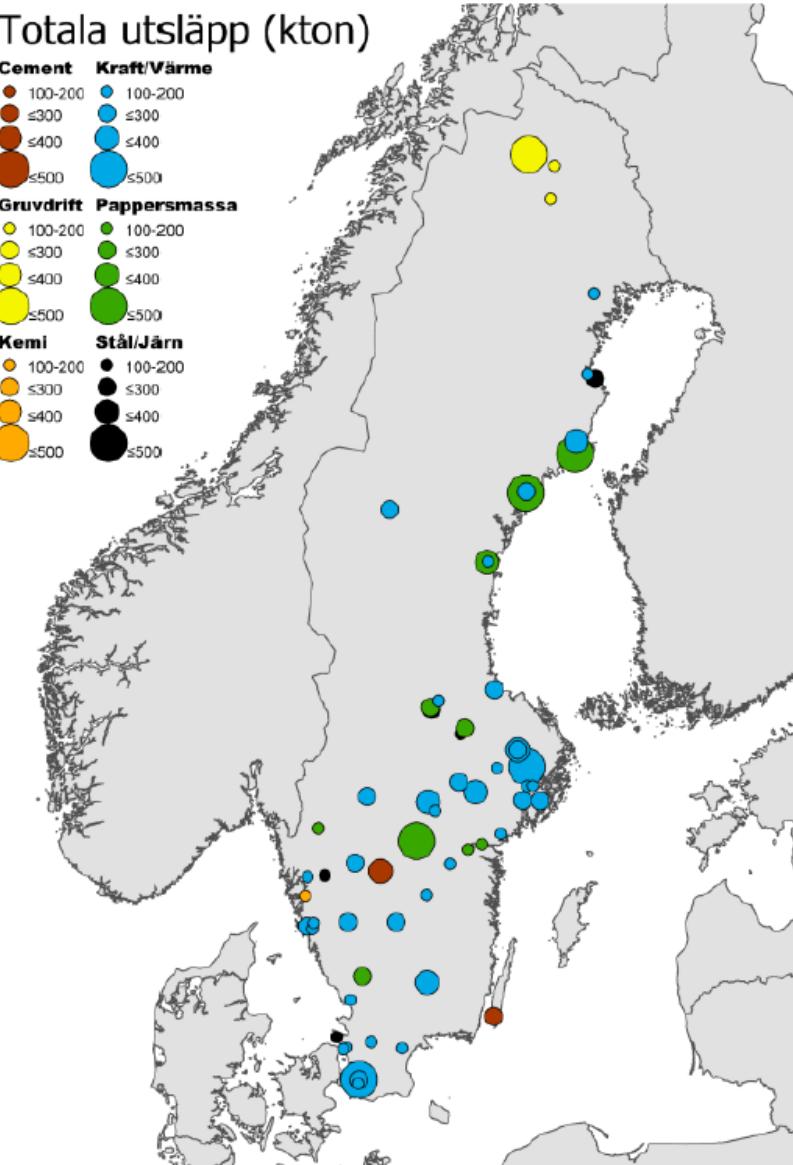
Gruvdrift Pappersmassa

- 100-200
- ≤300
- ≤400
- ≤500
- 100-200
- ≤300
- ≤400
- ≤500

Kemi Stål/Järn

- 100-200
- ≤300
- ≤400
- ≤500
- 100-200
- ≤300
- ≤400
- ≤500

Map source: Johnsson et al 2019



CO₂ utsläpp > 500 kt/år

Totala utsläpp (kton)

Raffinaderi Pappersmassa

- 500-750
- 1000
- ≤1500
- ≤2000
- 500-750
- ≤1000
- ≤1500
- ≤2000
- 500-750
- ≤1000
- ≤1500
- ≤2000
- 500-750
- ≤1000
- ≤1500
- ≤2000

Kemi Stål/Järn

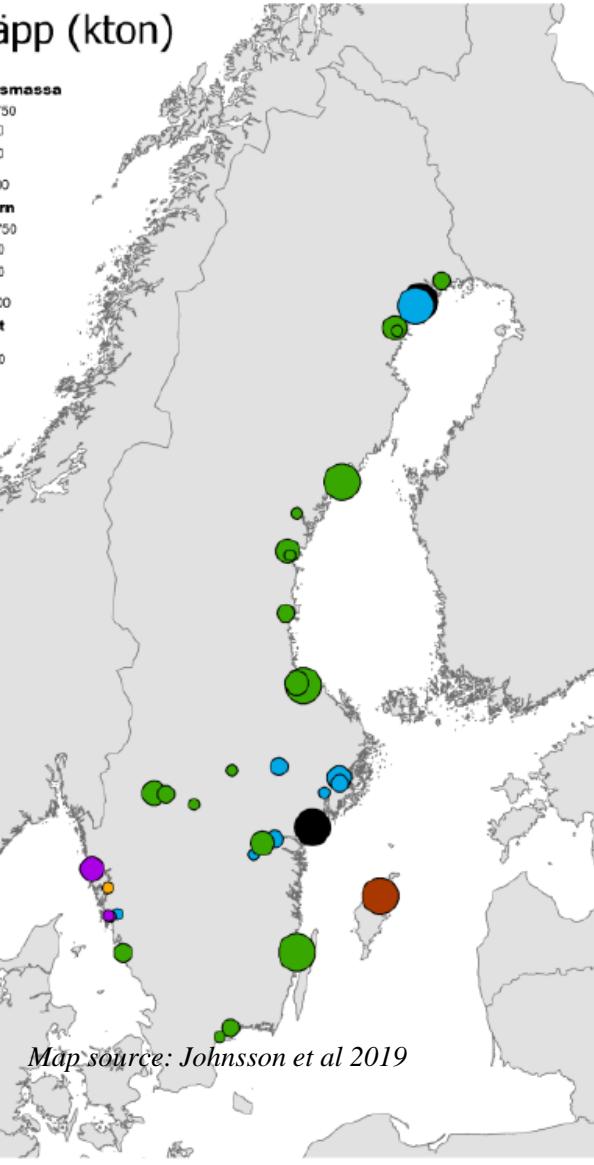
Kraft/Värme Cement

500-750

≤1000

≤1500

≤2000



Utsläpp
straffavgift år
2021= 1200kr /
ton

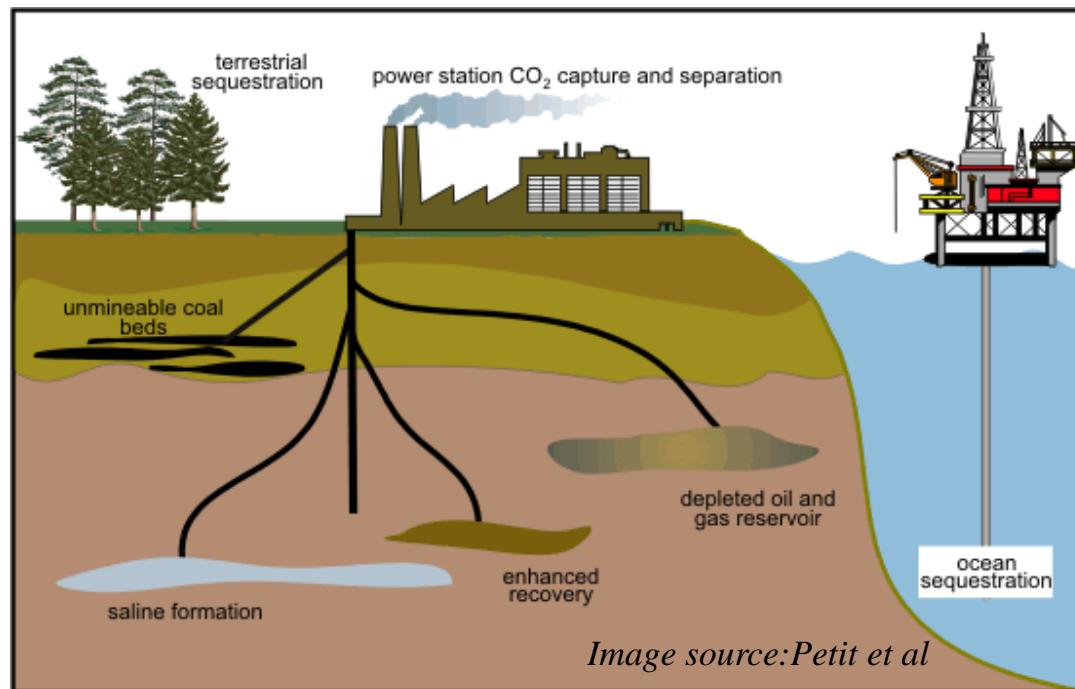
Utsläppen 2023 från anläggningarna (ej flyg) inom utsläppshandeln i Sverige var drygt 17,2 miljoner ton koldioxidekvivalenter, vilket innebär att utsläppen minskat med 2,4 procent från föregående år.

Major point source emitters of CO₂ in Sweden

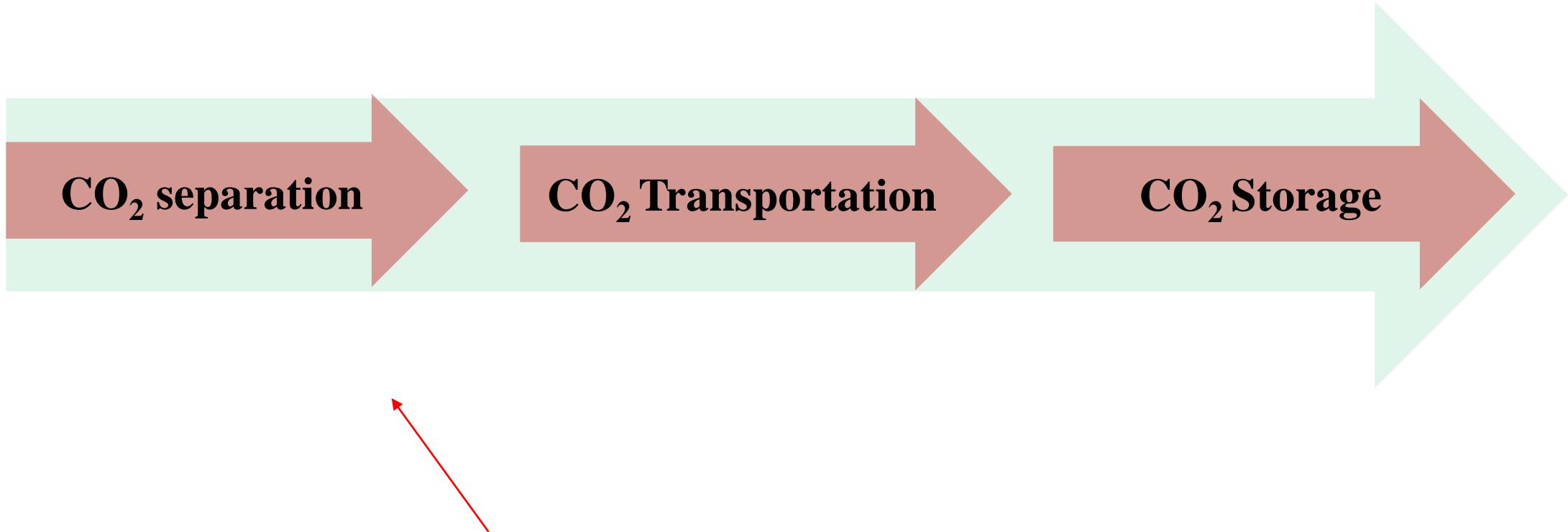
CO₂ separation

CO₂ Transportation

CO₂ Storage

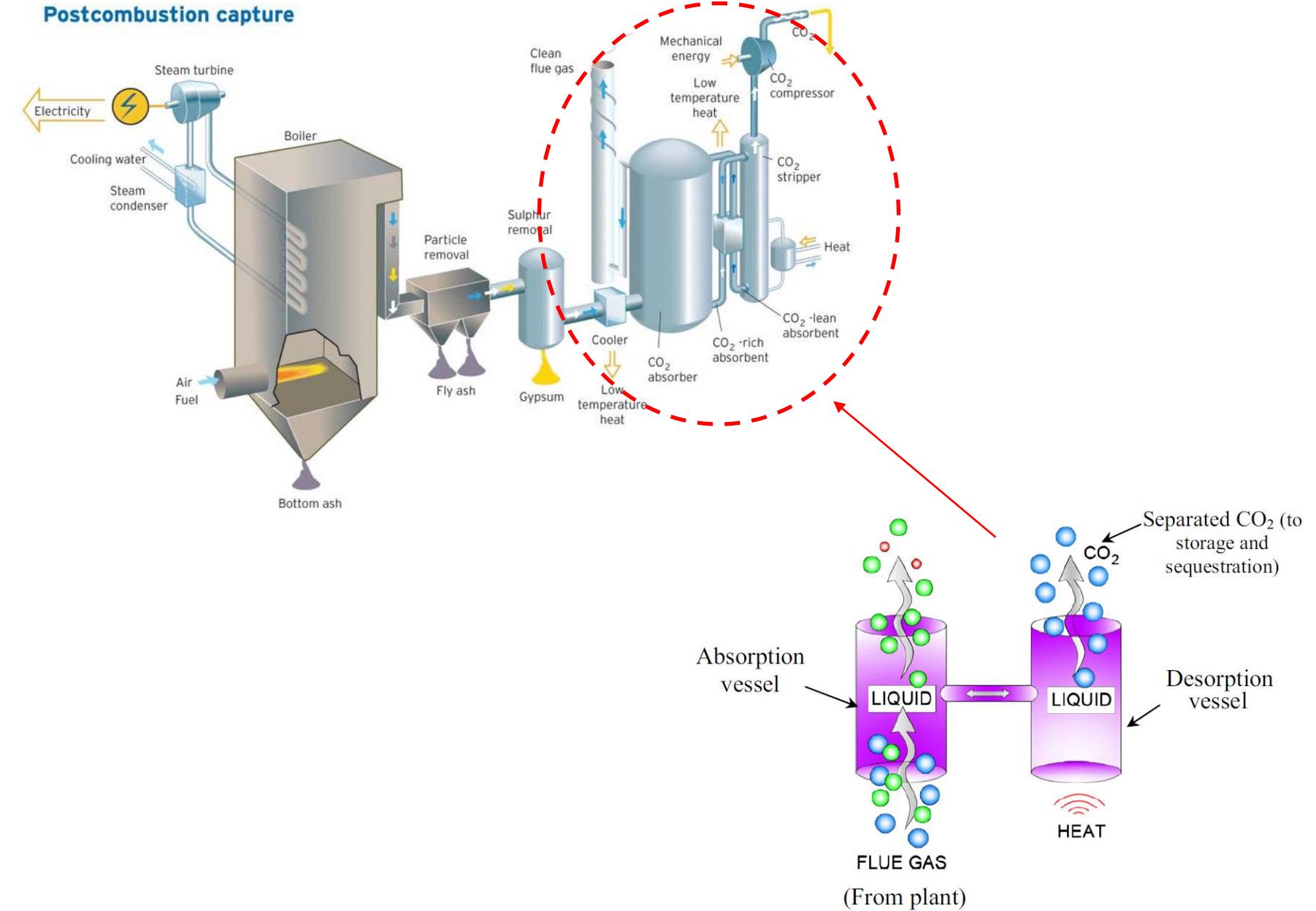


Geological CO₂ storage



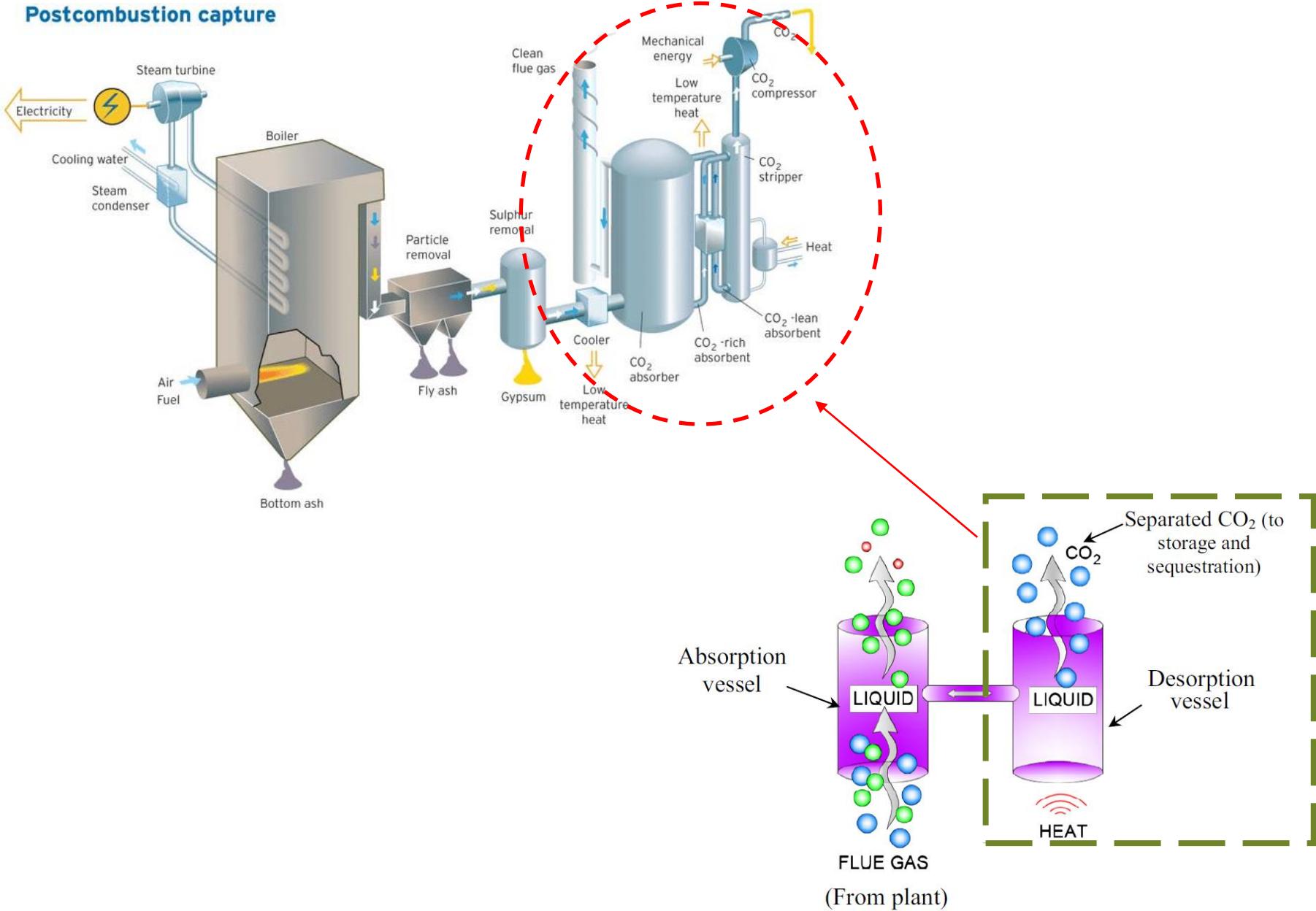
- *Accounts for 70 %–80 % of the overall bio-CCS (CCS) cost*
- *Thus, the development of a cost-efficient CO₂ separation process and material are crucial for the economic viability of bio-ccs*

Postcombustion capture



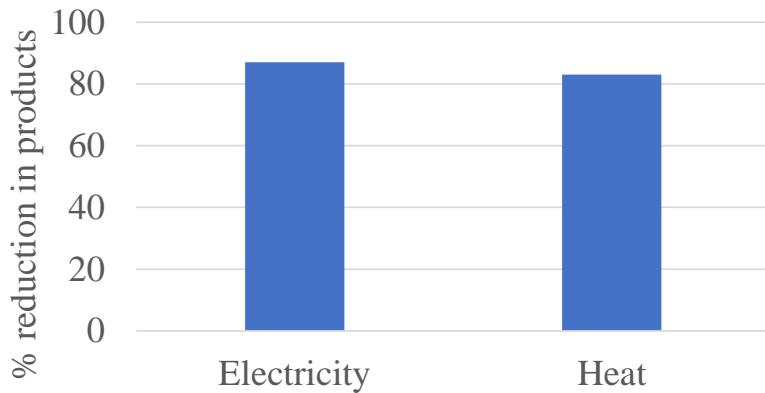
CO_2 separation benchmark: Chemical absorption with monoethanolamine (MEA)

Postcombustion capture

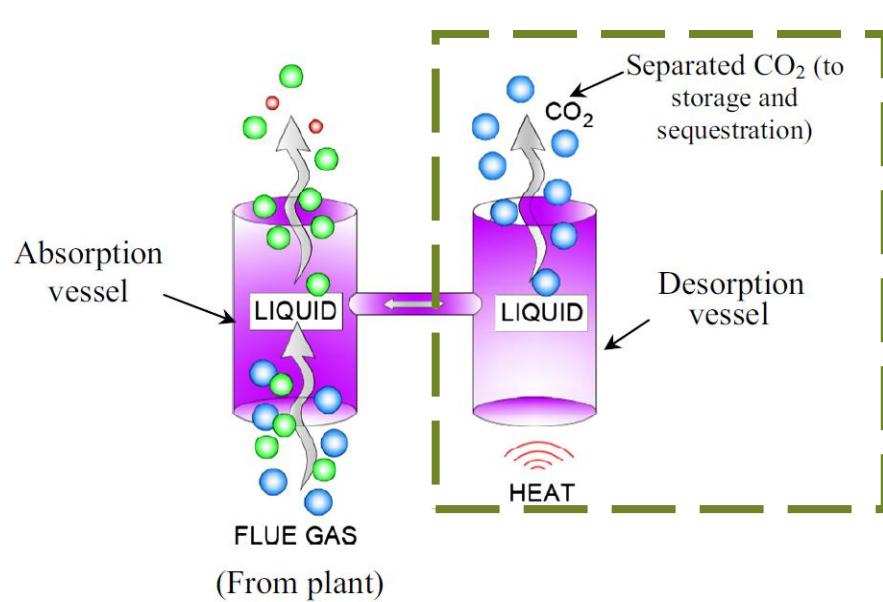


*Key problem:
Energy intensive regeneration:
3–6 GJ/tonne of CO₂*

CO₂ separation benchmark: Chemical absorption with monoethanolamine (MEA)



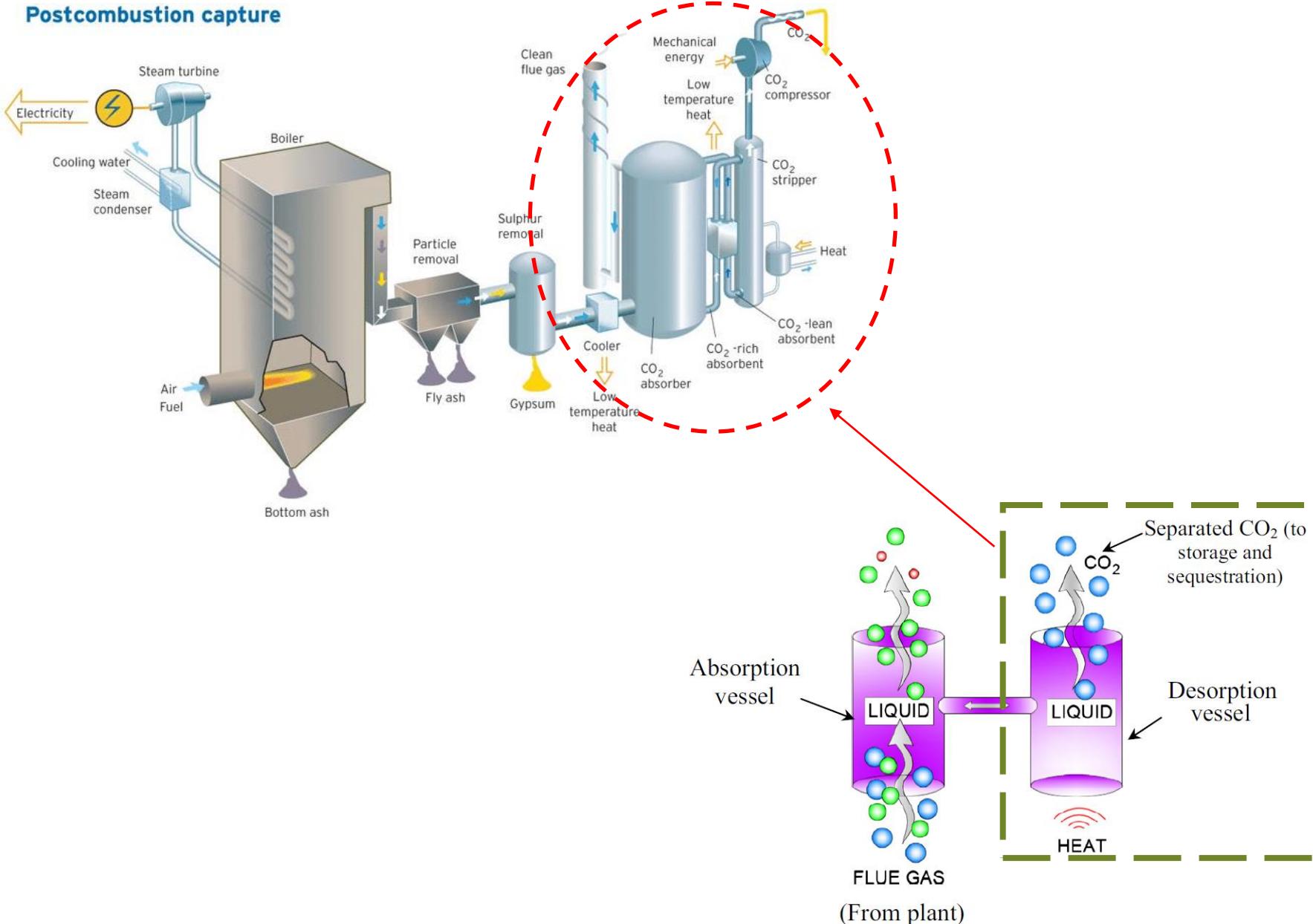
Percent reduction in the sale of electricity and heat
when MEA is applied for CO₂ separation



*Key problem:
Energy intensive regeneration:
3–6 GJ/tonne of CO₂*

CO₂ separation benchmark: Chemical absorption with monoethanolamine (MEA)

Postcombustion capture

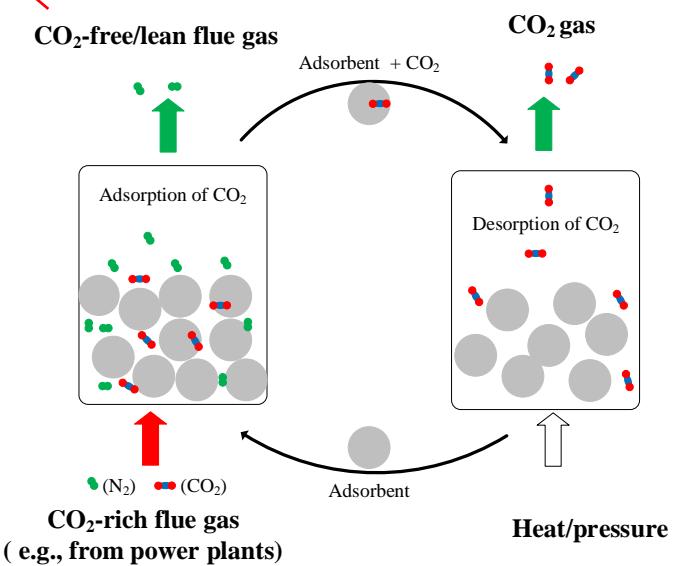
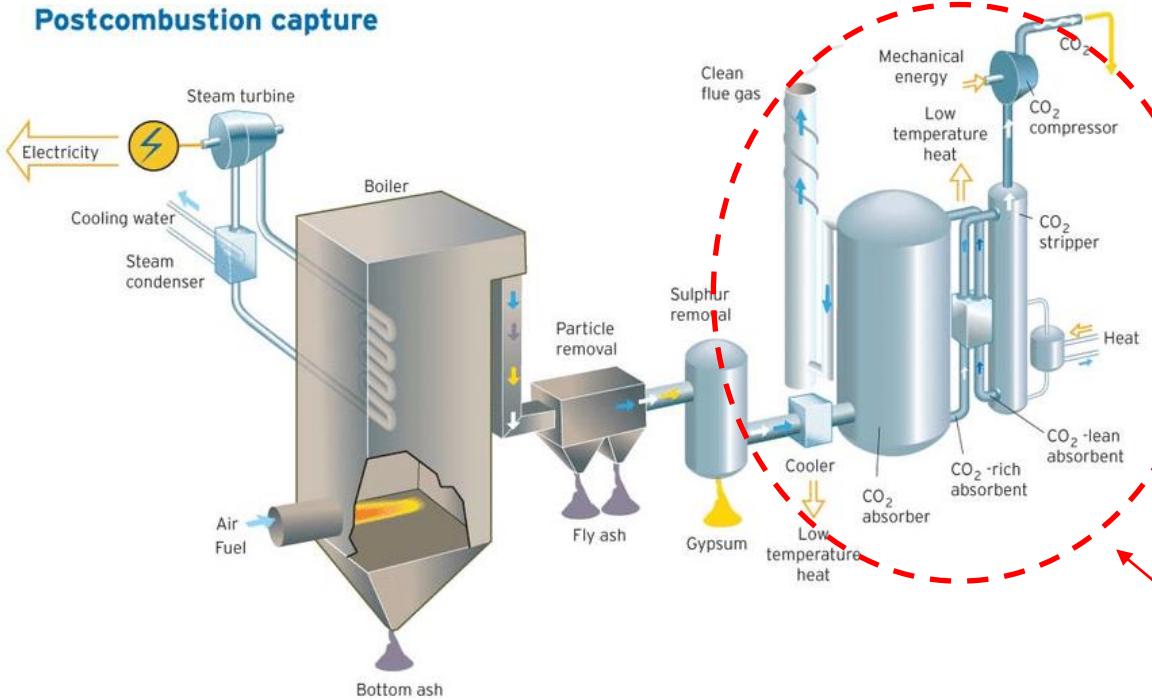


Key problem:
Energy intensive regeneration:
3–6 GJ/tonne of CO₂

Solution:
Energy demand for the regeneration step should < 2 GJ/tonne of CO₂ to enable the CO₂ separation process to be economically viable .

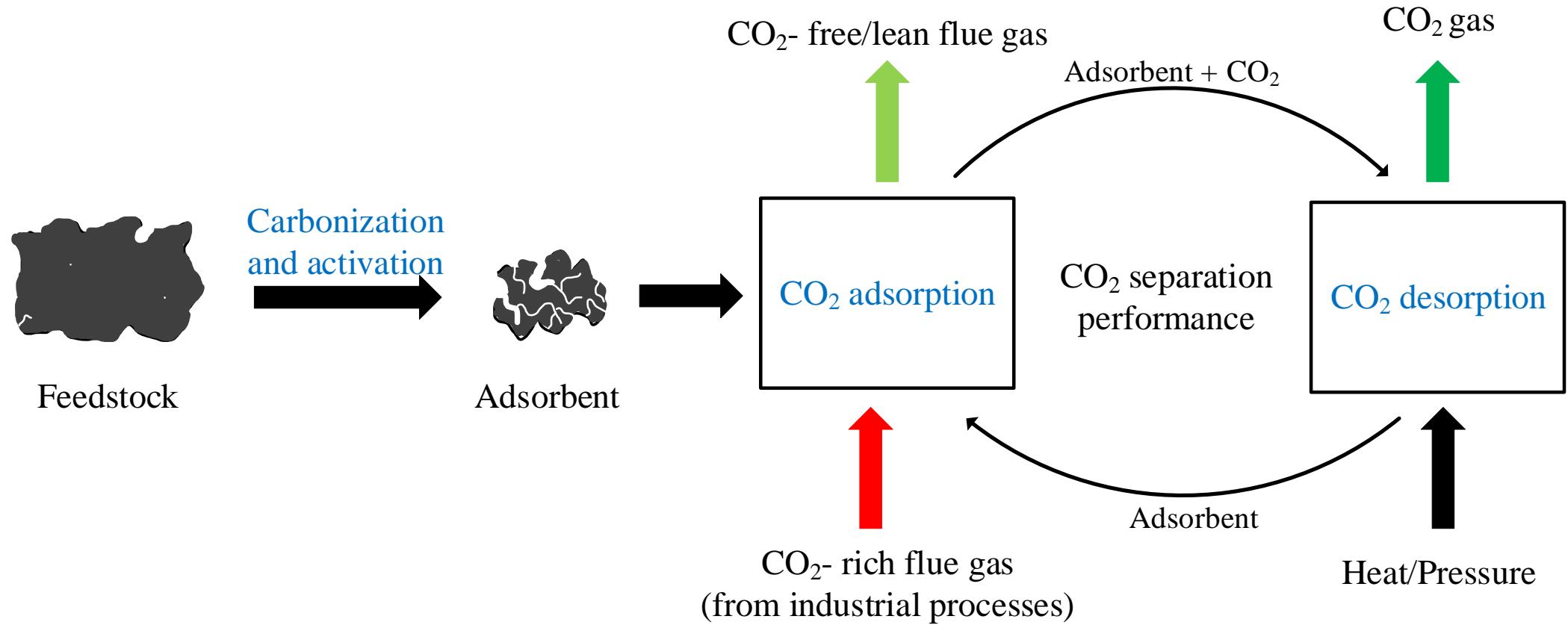
CO₂ separation benchmark: Chemical absorption with monoethanolamine (MEA)

Postcombustion capture



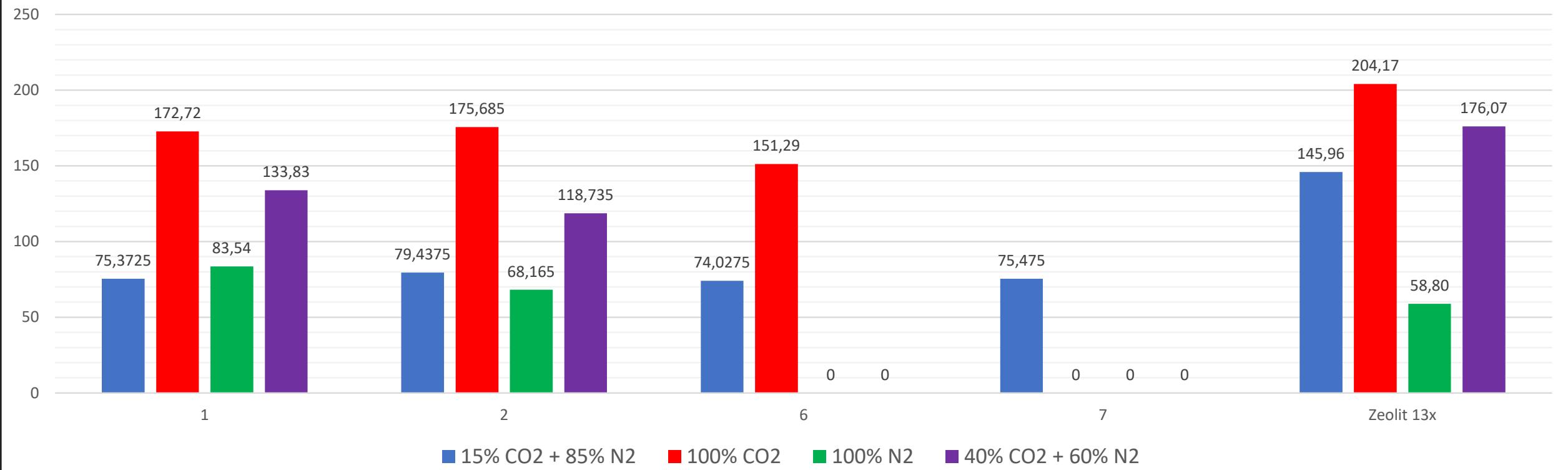
CO₂ separation by physical adsorption

Generally less energy intensive than MEA.

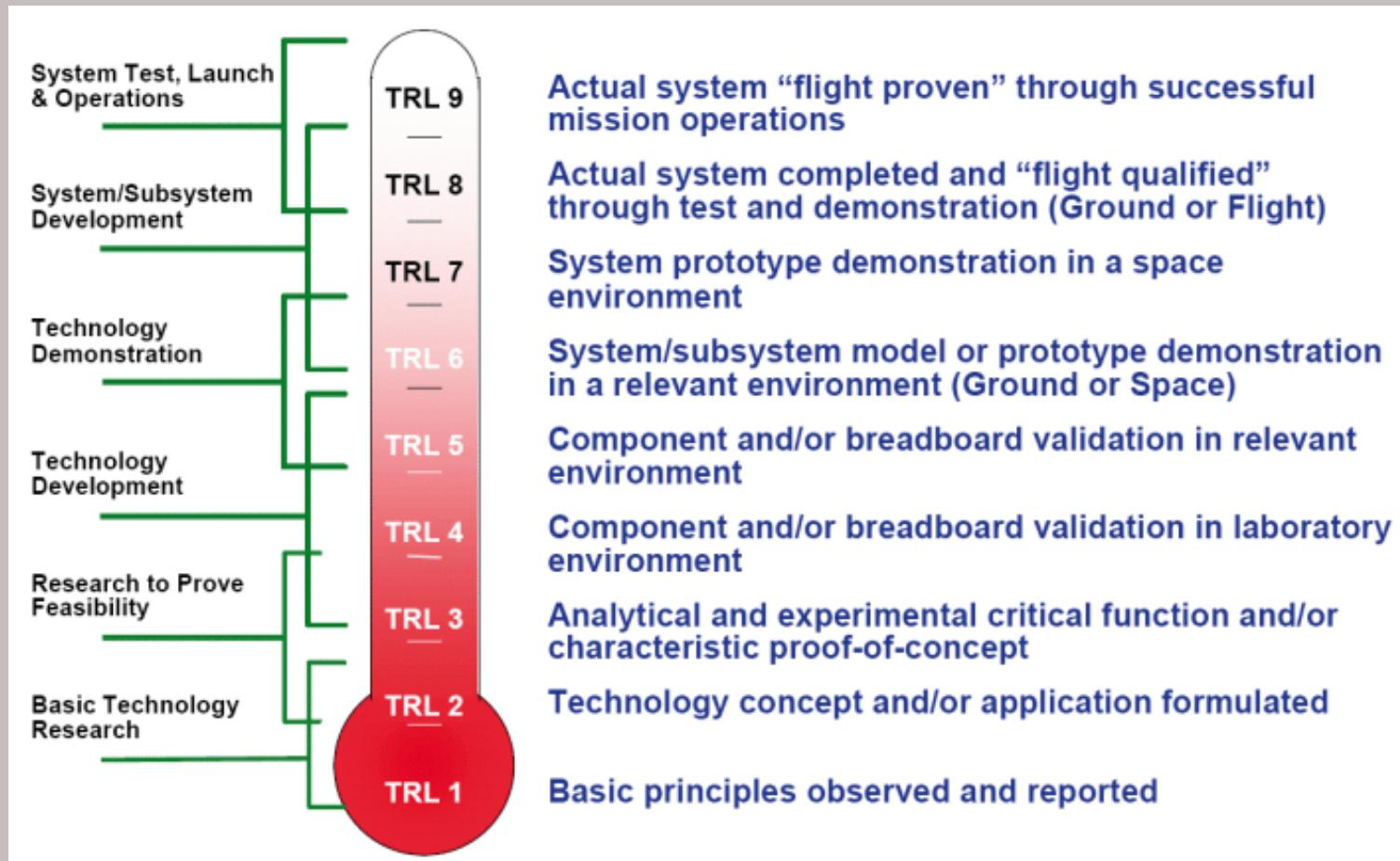


Proof of concept: *Can a CO₂ adsorbent be produced from polymer residues with a similar performance as commercial zeolites?*

Jämförelse mellan Adsorbenter



Titel förslag till projektet: Process optimisation of CO₂ separation for polymer based adsorbent-TRL3 to TRL4



Development of Cost-Efficient CO₂ Adsorbents from Low-value Polymers

RI.
SE

- Project partners:
 - Powerpipe systems AB (Jan Frick)
 - PUR Gruppen: Prio Plastic AB (Dragan Vasic)
 - Plixxent (Håkan Bengtsson)
 - Nässjö affärsverk AB (Andreas Lindahl)
 - RISE (Placid Atongka Tchoffor, Nazdaneh Yarahmadi, Anders Höije)



LoxiTec AB

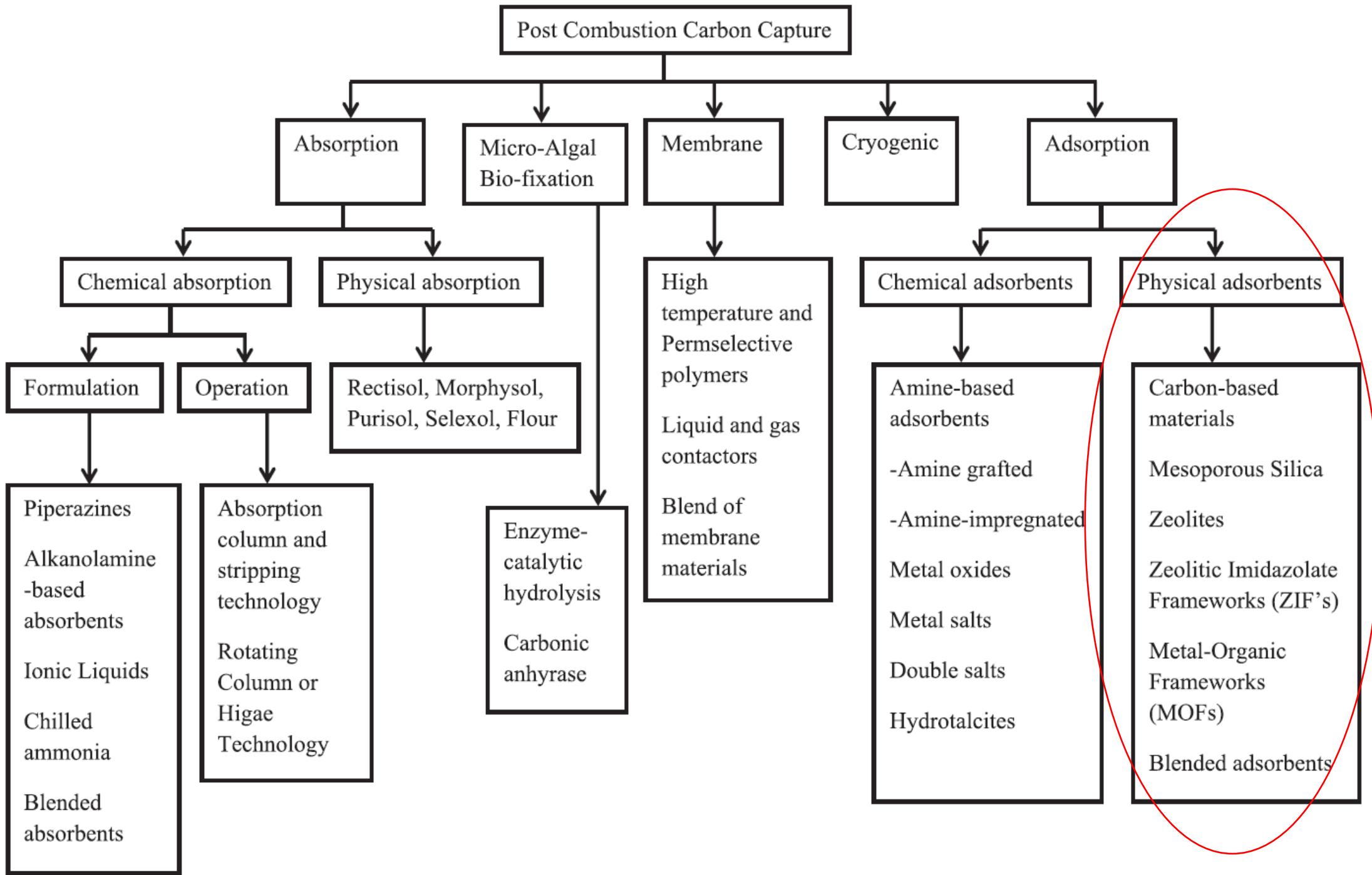
Financed by: Energimyndigheten – PUR gruppen, Powerpipe Systems AB, Nässjö Affärsverk AB

Project time: 2021-01-15 to ~~2022-02-30~~

2022-12-31

What will we do?

- Collaborate with PUR- gruppen
- Define optimum experimental conditions to produce CO₂ adsorbents from PUR and PIR waste from various products
- Evaluate the CO₂ separation performance of the produced CO₂ adsorbents
- Preliminary estimation of the cost to produce CO₂ adsorbents from PUR/PIR



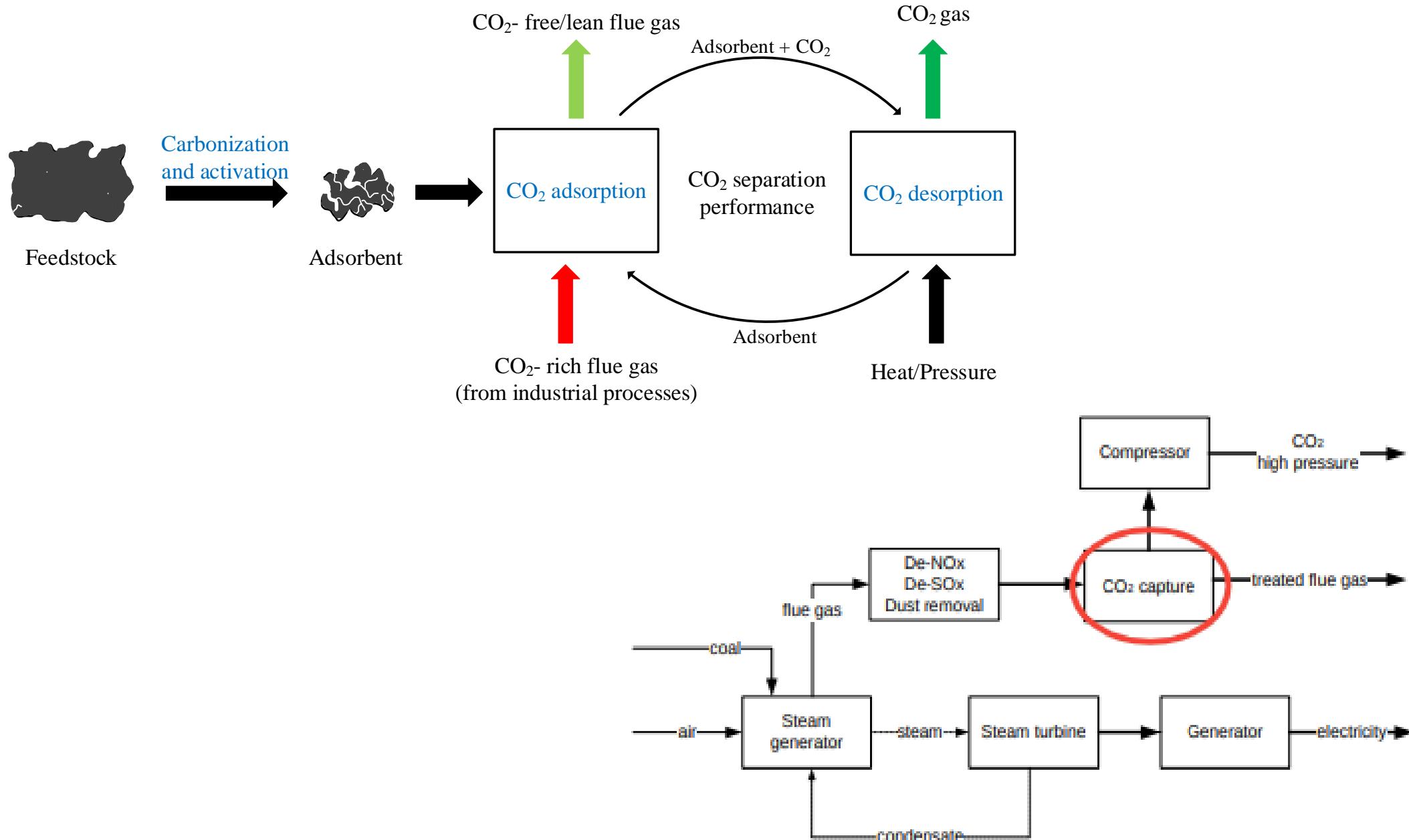


Fig.1. Schematic diagram of a power plant with post-combustion CO_2 capture [6]

Characterization and material selection

- PIR and PUR has been investigated with TGA to
 - Determine the amount of organic and inorganic parts
 - Determine thermal stability of the material



LX2, LX4, PIR and Power Pipe as well as zeolit for the reference material

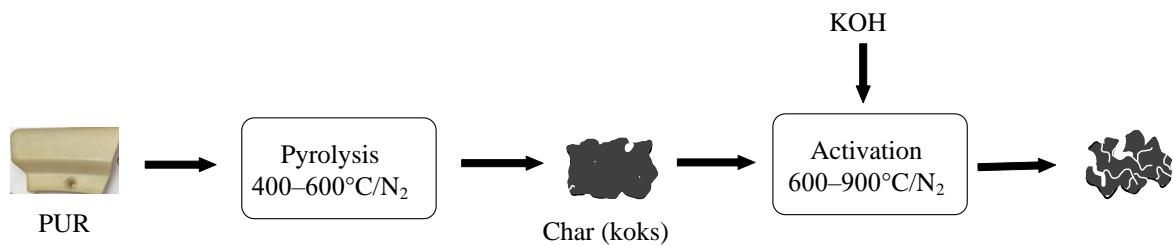


- Production of adsorbent
- Measuring the porosity

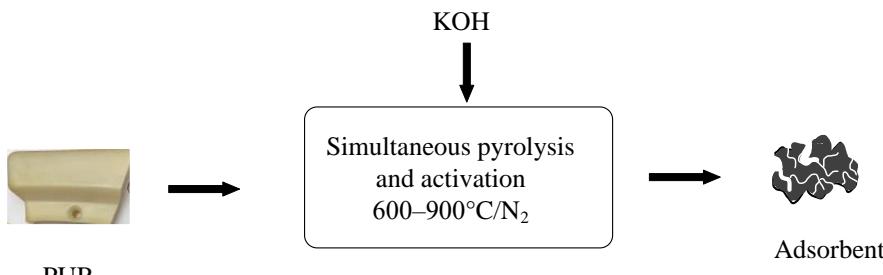
Find the correct
paramters and
production method
for the adsorbent

Adsorbent production (modification of the capacity of CO₂ by impregnation using K)

chemical production

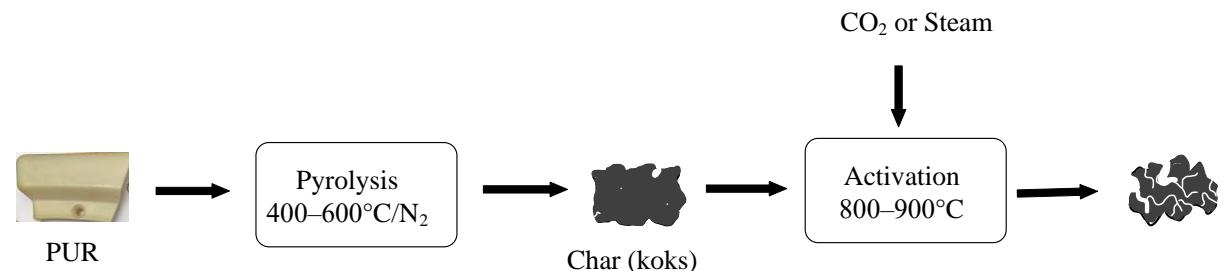


Indirect production of adsorbents by chemical activation

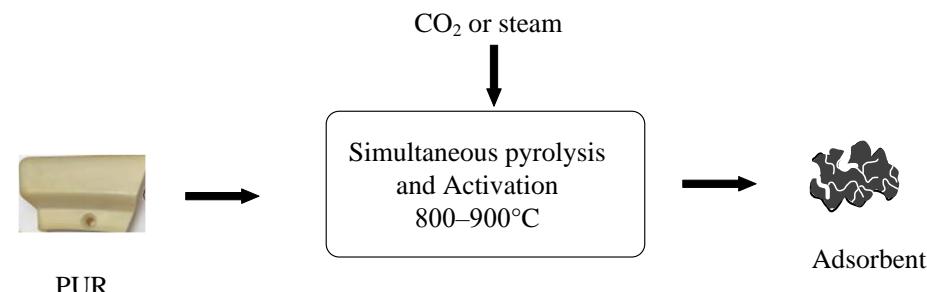


Direct production of adsorbents by chemical activation

physical production



Indirect production of adsorbents by physical activation

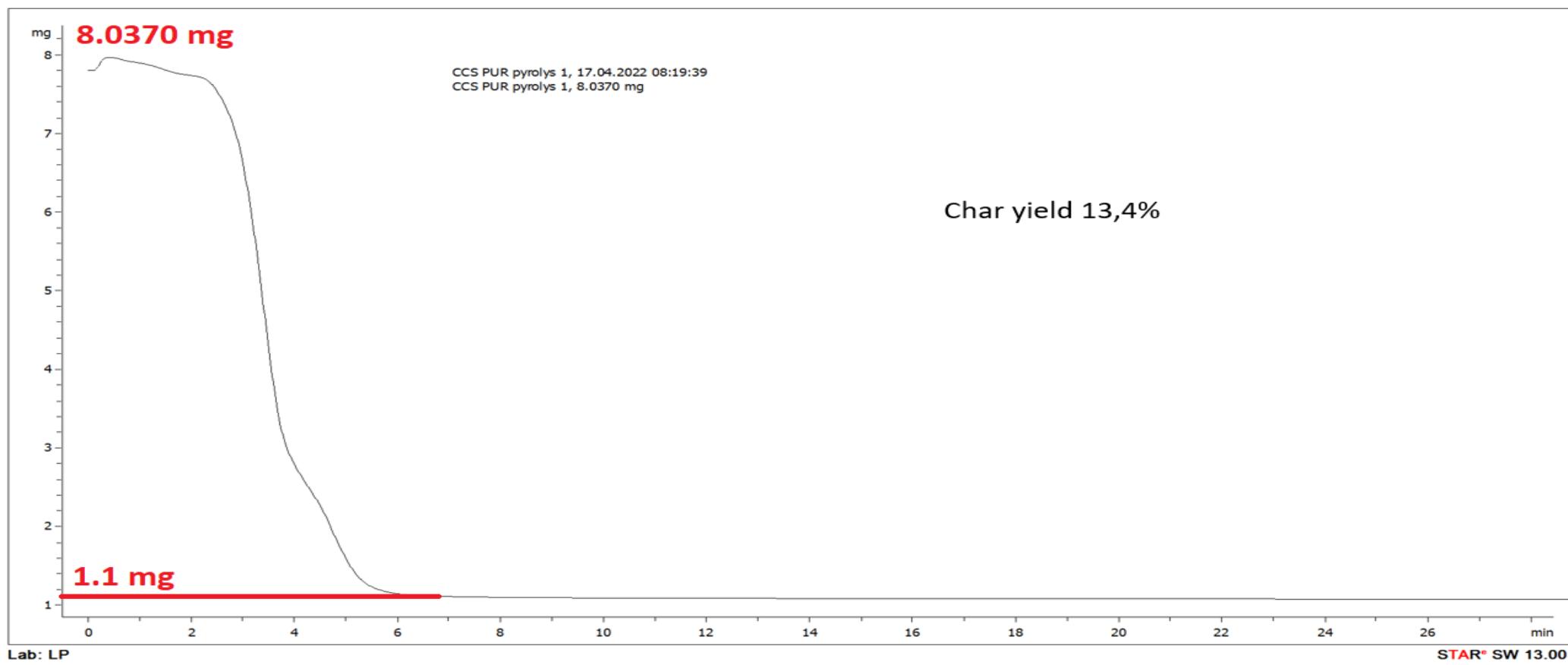


Direct production of adsorbents by physical activation

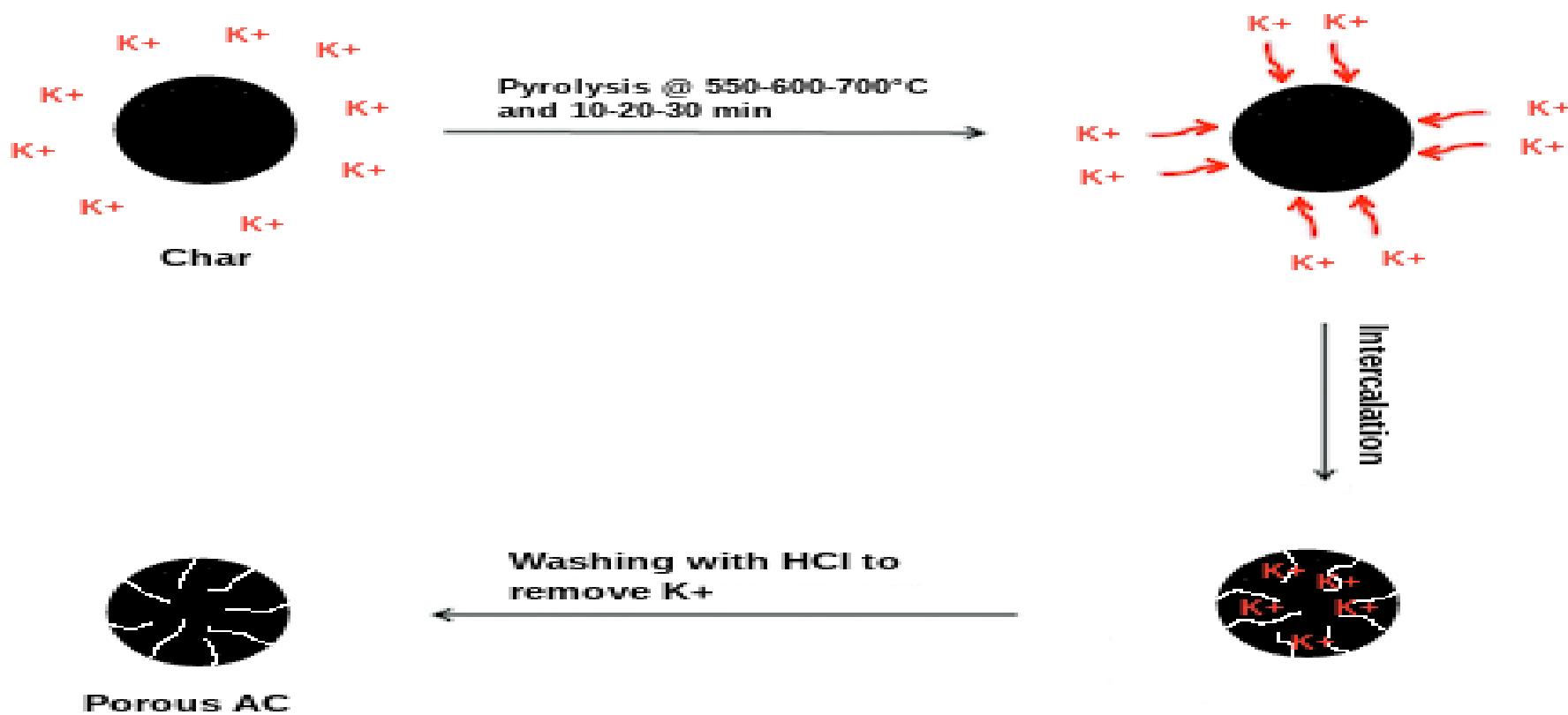
By altering time, temperature and KOH concentration

Run #	Sample	Activation method	K (m) ÷ Sample m)	Temperature, °C	time, min	N2 flow, ml/min	CO2 adsoption temp. °C
1	PUR	Indirect	0	650	20	200	25
2	PUR	Indirect	0,5	650	10	200	25
3	PUR	Indirect	0,5	650	20	200	25
4	PUR	Indirect	0,5	650	30	200	25
5	PUR	Indirect	0,5	550	Best time	200	25
6	PUR	Indirect	0,5	600	Best time	200	25
7	PUR	Indirect	0,5	700	Best time	200	25
8	PUR	Indirect	1	Best temp	Best time	200	25
9	PUR	Indirect	1,5	Best temp	Best time	200	25
10			Best C		Best time	200	25
11			1,5	650	Best time	200	25
12			1,5	700	Best time	200	25

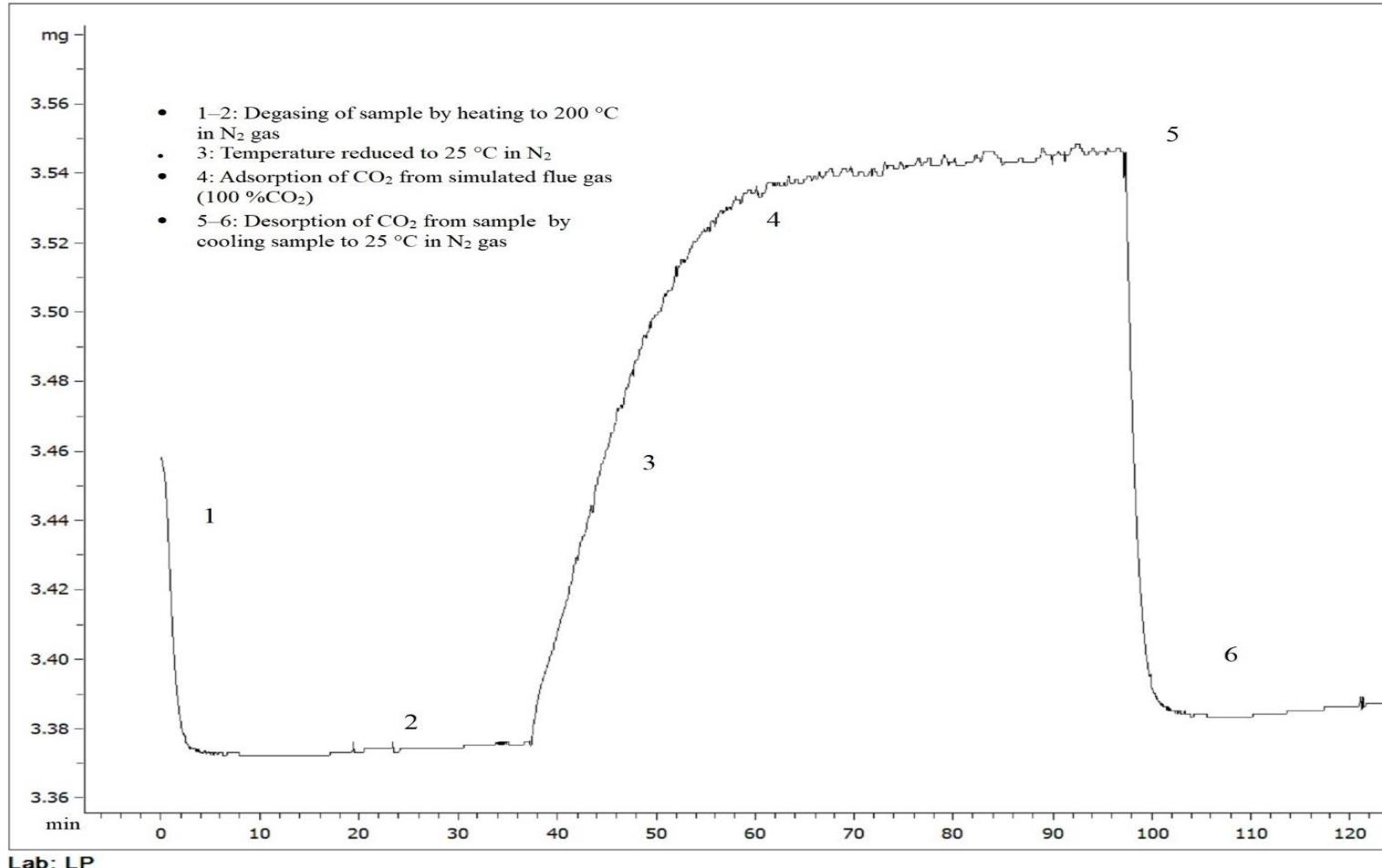
Char yield calculation by using TGA



KOH impact on char



Evaluation of adsorption and desorption by TGA



CO₂ adsorption evaluated by TGA

PUR, Indirect chemical activation

Run #	Sample	Activation method	K (m)÷ Sample m)	Temperature, °C	time, min	N2 flow, ml/min	CO2 adsoption temp. °C	Sample 1 (mg/g)	Sample 2 (mg/g)	Average
0	PUR	Indirect	0	650	20	200	25	51,17	51,24	51,2
1	PUR	Indirect	0,5	650	10	200	25	81,44	68,33	74,89
2	PUR	Indirect	0,5	650	20	200	25	66,55	77,46	72,01
3	PUR	Indirect	0,5	650	30	200	25	112,83	107,54	110,19
4	PUR	Indirect	0,5	650	40	200	25	49,42	68,2	58,81
5	PUR	Indirect	0,5	650	60	200	25	44,64	86,31	65,48
6	PUR	Indirect	0,5	550	30	200	25	38,09	31,55	34,82
7	PUR	Indirect	0,5	600	30	200	25	20,69		
8	PUR	Indirect	0,5	700	30	200	25	71,23	50,62	60,93
9	PUR	Indirect	1	650	30	200	25	73,02	95,52	84,27
10	PUR	Indirect	1,5	650	30	200	25	152,10	131,42	141,76

CO₂ adsorption evaluated by TGA

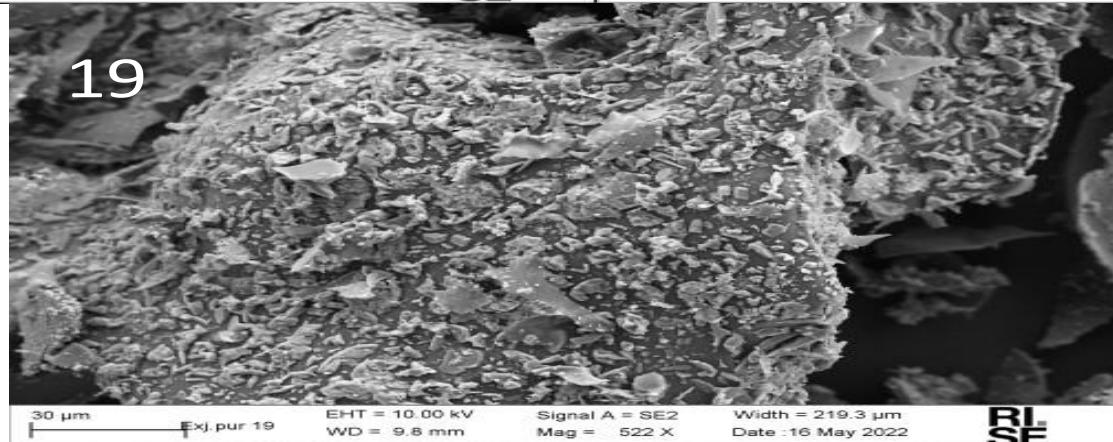
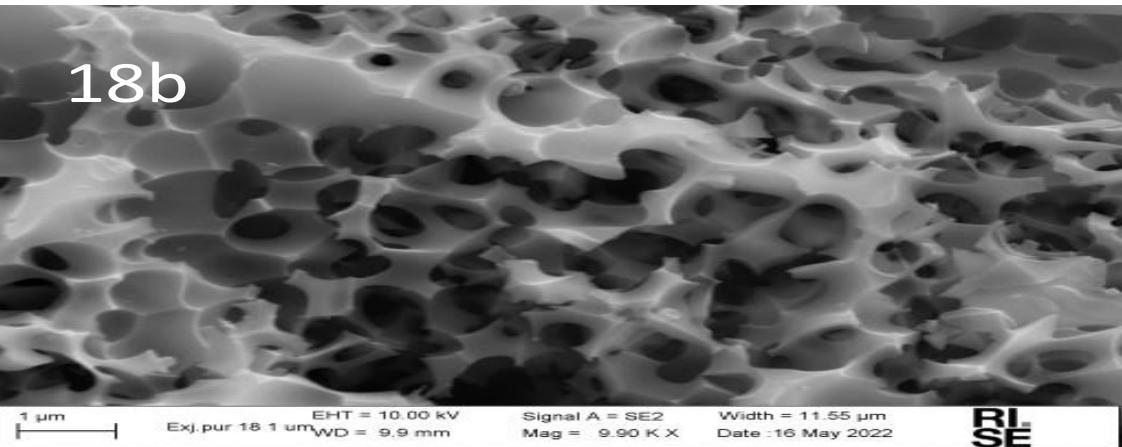
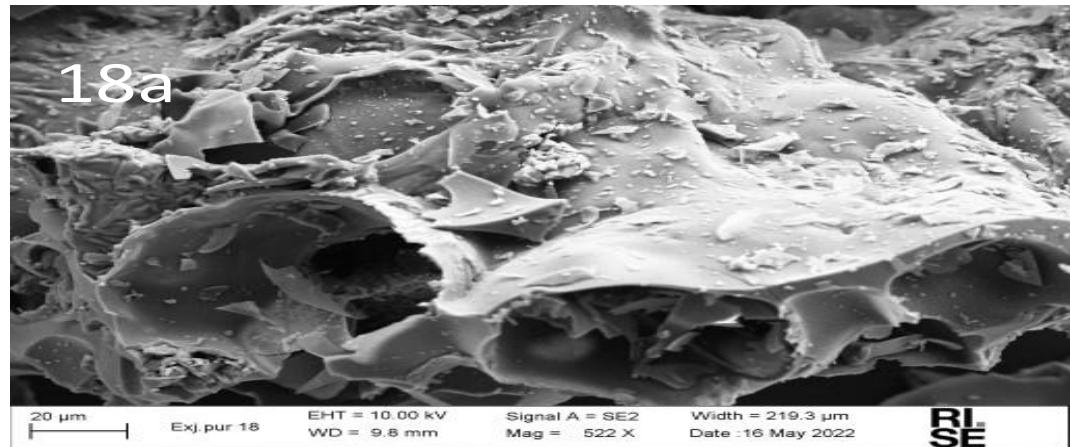
PUR, Direct Chemical activation

Run #	Sample	Activation method	K (m)÷ Sample m)	Temperature , °C	time, min	N2 flow, ml/min	CO2 adsoption temp. °C	Sample 1 (mg/g)	Sample 2 (mg/g)	Average
15	PUR	Direct	0,5	650	10	200	25			
16	PUR	Direct	0,5	650	20	200	25	93,86	92,42	93,14
17	PUR	Direct	0,5	650	30	200	25	95,06	100,36	97,71
18	PUR	Direct	0,5	650	40	200	25	115,48		115,48
19	PUR	Direct	0,5	650	50	200	25	53,32		53,32
20	PUR	Direct	0,5	650	60	200	25	90,36		
21	PUR	Direct	0,5	650	90	200	25	90,49		90,49
22	PUR	Direct	0,5	550	40	200	25	22,17		22,17
23	PUR	Direct	0,5	600	40	200	25	53,59		53,59
24	PUR	Direct	0,5	700	40	200	25	116,35		116,35
25	PUR	Direct	1	650	40	200	25	124,28		124,28
26	PUR	Direct	1,5	650	40	200	25	145,48		145,48
27	PUR	Direct	1,5	650	40	200	25	151,29		151,29

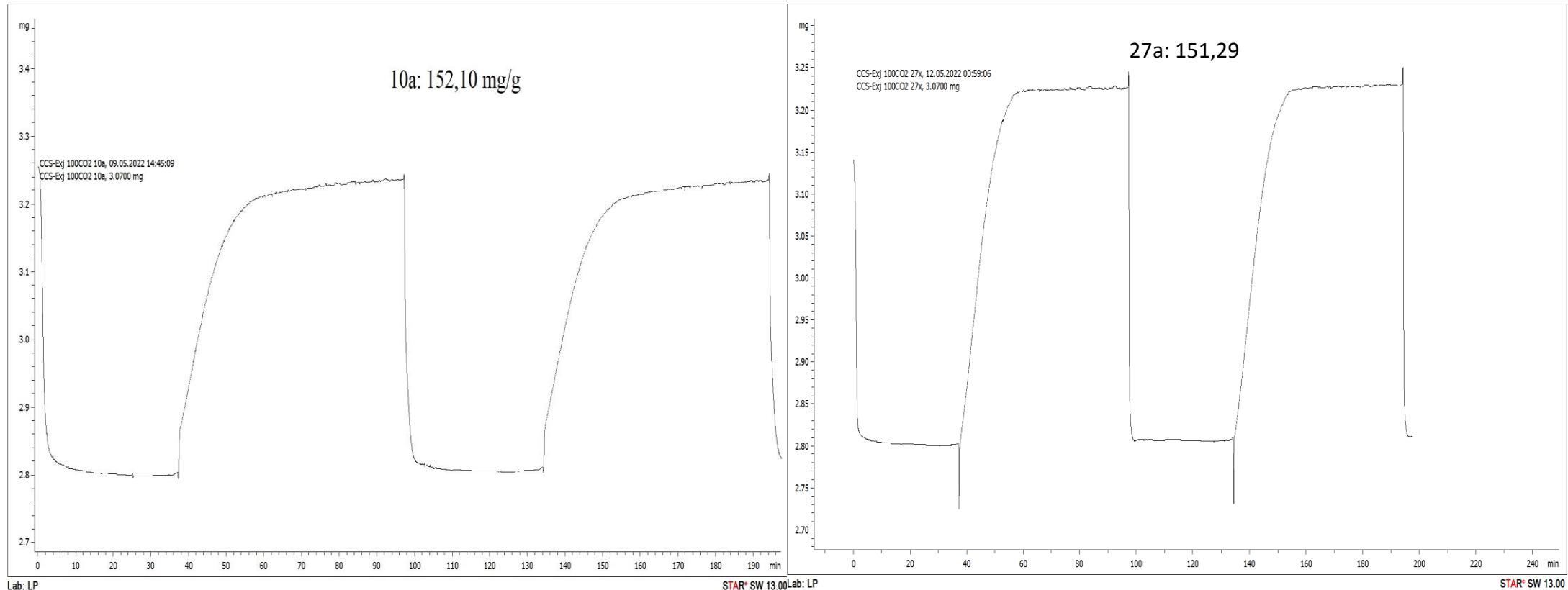
CO₂ adsorption evaluated by TGA PIR, Direct Chemical activation

Run #	Sample	K(m)÷Char(m)	Temp, °C	Time, min	15% CO ₂ + 85% N ₂			100% N ₂			40% CO ₂ + 60% N ₂			100% CO ₂		
					Sample 1	Sample 2	Average	Sample 1	Sample 2	Average	Sample 1	Sample 2	Average	Sample 1	Sample 2	Average
14	PIR	0	650	45	26,86	26,48	26,67	8,45	8,72	8,59	36,42	40,71	38,57	44,57	62,84	53,71
15	PIR	0,5	650	45	65,02	64,87	64,95	24,66	24,04	24,35	91,94	94,87	93,41	118,18	133,82	126,00
16	PIR	0,5	650	90	55,92	58,19	57,06	21,75	22,93	22,34	83,00	85,29	84,15	103,88	126,13	115,01
17	PIR	0,5	650	20	71,26	72,18	71,72	26,72	26,99	26,86	106,62	110,94	108,78	137,73	157,41	147,57
21	PIR	0,5	700	45	100,94	98,55	99,75	65,24	59,66	62,45	88,22	92,28	90,25	122,08	153,88	137,98
22	PIR	1,5	600	45	116,33	104,51	110,42	70,19	65,90	68,05	104,66	112,55	108,61	142,32	161,93	152,13
23	PIR	1,5	650	45	110,11	111,13	110,62	65,79	70,54	68,17	116,07	121,40	118,74	170,73	180,64	175,69
24	PIR	1,5	700	45	99,76	96,47	98,12	63,34	64,73	64,04	98,12	105,47	101,80	161,97	185,84	173,91
25	PIR	1	600	45	119,29	129,42	124,36	70,45	71,87	71,16	117,36	129,64	123,50	155,27	174,96	165,12
26	Zeolite 13X				146,78	145,14	145,96	51,23	66,37	58,80	180,40	171,73	176,07	205,13	203,21	204,17
27	PIR	1,5	600	20				37,96	35,28	36,62	104,40	114,25	109,33	156,43	156,27	156,35
28	PIR	1,5	650	20				80,79	86,29	83,54	119,88	147,78	133,83	170,77	174,67	172,72
29	PIR	1,5	700	20				77,64		77,64	116,12	158,82	137,47	166,22	165,21	165,72
30	PIR	0,5	600	45				34,8	34,34	34,57	80,94	91,98	86,46	112,94	112,08	112,51
31	PIR	0,5	600	90				36,5	36,37	36,44	94,82	90,63	92,73	130,82	128,97	129,90
32	PIR	0,5	600	20				32,59	31,4	32,00	82,15	76,82	79,49	112,69	113,98	113,34
33	PIR	0,5	600	180				38,84	38,56	38,70				133,87	133,25	133,56
34	PIR	1	600	180				45,39	46,72	46,06				155,66	154,68	155,17
35	PIR	1	600	90				51,46	52,35	51,91				168,97	168,62	168,80
36	PIR	1	650	20				43,63	44,87	44,25				147,16	148,05	147,61

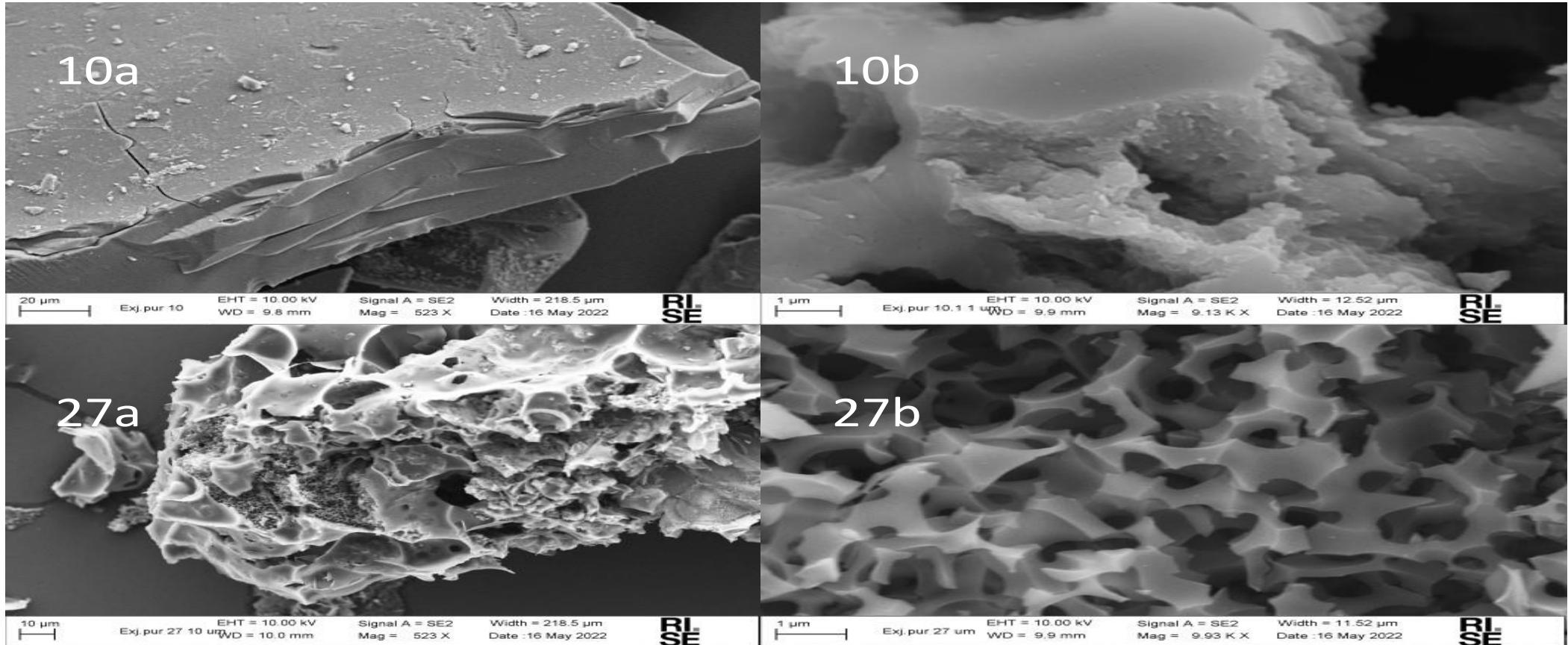
Comparison of surface between sample 18 and 19 using SEM



Comparison between the best samples with the optimum parameters using TGA from indirect and direct activation methods



Comparison of surface between sample from indirect and direct activation using SEM



Summary

- Results show difference in surface structure between indirect and direct activation
- Similar CO₂ adsorption capacity between indirect and direct activation
- The PIR material adsorbent produced by 1,5 K/char ratio at 650 C during 45 minutes has shown best CO₂ capture capacity corresponding 175,7mg/g compare to Zeolit 13X for 204mg/g